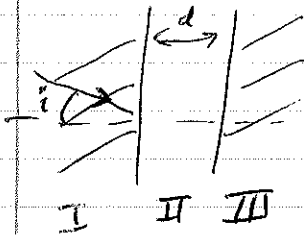


(a) only.

7.3 Two plane semi-infinite slabs of the same uniform isotropic nonpermeable lossless dielectric with index of refraction n are parallel and separated by an air gap ($n=1$) of width d . A plane electromagnetic wave of frequency ω is incident on the gap from one of the slabs with angle of incidence i . For linear polarizations both parallel to and perpendicular to the plane of incidence,

a) calculate the ratio of power transmitted into the second slab to the incident power & the ratio of reflected to incident power.



We write

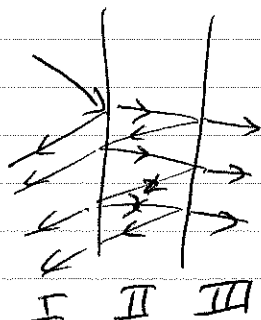
$$\vec{E}_I = \vec{E}_0 E_0 e^{i(\frac{n}{c} \omega \hat{h} \cdot \vec{x} - \omega t)} + \vec{E}_1 E_1 e^{i(\frac{n}{c} \omega_1 \hat{h}_1 \cdot \vec{x} - \omega_1 t)}$$

$$\vec{E}_{II} = \vec{E}_2 E_2 e^{i(\frac{1}{c} \omega_2 \hat{h}_2 \cdot \vec{x} - \omega_2 t)} + \vec{E}_3 E_3 e^{i(\frac{1}{c} \omega_3 \hat{h}_3 \cdot \vec{x} - \omega_3 t)}$$

$$\vec{E}_{III} = \vec{E}_4 E_4 e^{i(\frac{n}{c} \omega_4 \hat{h}_4 \cdot (\vec{x} - \vec{d}) - \omega_4 t)}$$

Here $\hat{h} = \frac{\vec{h}}{|\vec{h}|}$,
not necessarily \hat{z} .

$\vec{E}_0 E_0$ corresponds to the original incoming wave. The other terms are all sums of contributions from all possible reflections.



7.3 a) cont'd

Since the boundary conditions must hold at all times & all positions on the boundary,

$$e^{i(\frac{n}{c} \omega \hat{h}_1 \cdot \vec{x} - \omega t)} \Big|_{z=0} = e^{i(\frac{n}{c} \omega_1 \hat{h}_1 \cdot \vec{x} - \omega_1 t)} \Big|_{z=0}$$

$$= e^{i(\frac{1}{c} \omega_2 \hat{h}_2 \cdot \vec{x} - \omega_2 t)} \Big|_{z=0} = e^{i(\frac{1}{c} \omega_3 \hat{h}_3 \cdot \vec{x} - \omega_3 t)} \Big|_{z=0}$$

$$\& e^{i(\frac{1}{c} \omega_2 \hat{h}_2 \cdot \vec{x} - \omega_2 t)} \Big|_{z=d} = e^{i(\frac{1}{c} \omega_3 \hat{h}_3 \cdot \vec{x} - \omega_3 t)} \Big|_{z=d}$$

$$= e^{i(\frac{n}{c} \omega_4 \hat{h}_4 \cdot (\vec{x} - d\hat{z}) - \omega_4 t)} \Big|_{z=d}$$

Since these conditions must hold for all t ,
the coefficients of t must match separately,

$$\Rightarrow \omega = \omega_1 = \omega_2 = \omega_3 = \omega_4$$

That leaves

$$n \hat{h} \cdot \vec{x} \Big|_{z=0} = n \hat{h}_1 \cdot \vec{x} \Big|_{z=0} = \hat{h}_2 \cdot \vec{x} \Big|_{z=0} = \hat{h}_3 \cdot \vec{x} \Big|_{z=0}$$

$$\hat{h}_2 \cdot \vec{x} \Big|_{z=d} = \hat{h}_3 \cdot \vec{x} \Big|_{z=d} = n \hat{h}_4 \cdot (\vec{x} - d\hat{z}) \Big|_{z=d}$$

Assume the plane of incidence is aligned with the xz plane,
so that none of these vectors has any y dependence.

Taking x components,

$$n \sin \theta_i = n \sin \theta_1 = \sin \theta_2 = \sin \theta_3$$

$$\sin \theta_2 = \sin \theta_3 = n \sin \theta_4$$

$$\Rightarrow \theta_i = \theta_1, \quad \theta_2 = \theta_3, \quad n \sin \theta_i = \sin \theta_2 = n \sin \theta_4$$

2.3 a), cont'd

We can now rewrite the eqns for the fields:

$$\vec{E}_I = \bar{\epsilon}_0 E_0 e^{i\left(\frac{n}{c}\omega(x \sin\theta_i + z \cos\theta_i) - \omega t\right)} + \bar{\epsilon}_1 E_1 e^{i\left(\frac{n}{c}\omega(x \sin\theta_i - z \cos\theta_i) - \omega t\right)}$$

$$\vec{E}_{II} = \bar{\epsilon}_2 E_2 e^{i\left(\frac{1}{c}\omega(x n \sin\theta_i + z \sqrt{1-n^2 \sin^2\theta_i}) - \omega t\right)} + \bar{\epsilon}_3 E_3 e^{i\left(\frac{1}{c}\omega(x n \sin\theta_i - z \sqrt{1-n^2 \sin^2\theta_i}) - \omega t\right)}$$

$$\vec{E}_{III} = \bar{\epsilon}_4 E_4 e^{i\left(\frac{n}{c}\omega(x \sin\theta_i + (z-d) \cos\theta_i) - \omega t\right)}$$

For simplicity, let us restrict to $x=0$ and $t=0$.

$$\vec{E}_I = \bar{\epsilon}_0 E_0 e^{i\frac{n}{c}\omega z \cos\theta_i} + \bar{\epsilon}_1 E_1 e^{-i\frac{n}{c}\omega z \cos\theta_i}$$

$$\vec{E}_{II} = \bar{\epsilon}_2 E_2 e^{i\frac{1}{c}\omega z \cos\theta_2} + \bar{\epsilon}_3 E_3 e^{-i\frac{1}{c}\omega z \cos\theta_2}$$

$$\vec{E}_{III} = \bar{\epsilon}_4 E_4 e^{i\frac{n}{c}\omega(z-d) \cos\theta_i}$$

$$\text{where } \cos\theta_2 = \sqrt{1-n^2 \sin^2\theta_i}$$

7.3 d), cont'd

Polarization perpendicular to plane of incidence:

~~$$\vec{A} = \vec{E}_0 = \vec{E}_1 = \vec{E}_2 = \vec{E}_3 = \vec{E}_4 = \hat{y} = \hat{j}$$~~

$$\vec{E}_0 = \vec{E}_1 = \vec{E}_2 = \vec{E}_3 = \vec{E}_4 = \hat{y} = \hat{j}$$

$$\vec{B} = \frac{n}{c} \hat{i} \times \vec{E}$$

$$\vec{B}_I = \frac{n}{c} (\sin \theta_i \hat{z} - \cos \theta_i \hat{x}) E_0 e^{i \frac{n}{c} \omega z \cos \theta_i}$$

$$+ \frac{n}{c} (\sin \theta_i \hat{z} + \cos \theta_i \hat{x}) E_1 e^{-i \frac{n}{c} \omega z \cos \theta_i}$$

$$\vec{B}_{II} = \frac{1}{c} (n \sin \theta_i \hat{z} - \cos \theta_2 \hat{x}) E_2 e^{i \frac{1}{c} z \cos \theta_2}$$

$$+ \frac{1}{c} (n \sin \theta_i \hat{z} + \cos \theta_2 \hat{x}) E_3 e^{-i \frac{1}{c} z \cos \theta_2}$$

$$\vec{B}_{III} = \frac{n}{c} (\sin \theta_i \hat{z} - \cos \theta_i \hat{x}) E_4 e^{i \frac{n}{c} \omega (z-d) \cos \theta_i}$$

Boundary conditions: (analogous of (7.37))

~~AA $\vec{E}_I \cdot \hat{z} = \vec{E}_{II} \cdot \hat{z}$~~

$$\textcircled{1} \left. \epsilon_1 \vec{E}_I \cdot \hat{z} \right|_{z=0} = \left. \epsilon_0 \vec{E}_{II} \cdot \hat{z} \right|_{z=0}, \quad \textcircled{2} \left. \vec{E}_I \times \hat{z} \right|_{z=0} = \left. \vec{E}_{II} \times \hat{z} \right|_{z=0}$$

$$\textcircled{3} \left. \vec{B}_I \cdot \hat{z} \right|_{z=0} = \left. \vec{B}_{II} \cdot \hat{z} \right|_{z=0}, \quad \textcircled{4} \left. \vec{B}_I \times \hat{z} \right|_{z=0} = \left. \vec{B}_{II} \times \hat{z} \right|_{z=0}$$

& similarly at $z=d$.Since the materials are nonmagnetic, we assume $\mu = \mu_0$ everywhere,
hence $\epsilon_1 / \epsilon_0 = n^2$.

7.3 a), cont'd

Polarization \perp plane of incidence, cont'dat $z=0$,

① $\Rightarrow \partial = 0$

② $\Rightarrow E_0 + E_1 = E_2 + E_3$

③ $\Rightarrow n \sin \theta_i (E_0 + E_1) = n \sin \theta_i (E_2 + E_3)$, same as above

④ $\Rightarrow n \cos \theta_i (-E_0 + E_1) = \cos \theta_2 (-E_2 + E_3)$

at $z=d$,

① $\Rightarrow \partial = 0$

② $\Rightarrow E_2 e^{i\frac{\omega}{c}d \cos \theta_2} + E_3 e^{-i\frac{\omega}{c}d \cos \theta_2} = E_4$

③ $\Rightarrow n \sin \theta_i (E_2 e^{i\frac{\omega}{c}d \cos \theta_2} + E_3 e^{-i\frac{\omega}{c}d \cos \theta_2}) = n \sin \theta_i E_4$, same as above

④ $\Rightarrow \cos \theta_2 (-E_2 e^{i\frac{\omega}{c}d \cos \theta_2} + E_3 e^{-i\frac{\omega}{c}d \cos \theta_2}) = -n \cos \theta_i E_4$

After a lot of algebra, one can show

$$\frac{E_1}{E_0} = \frac{(1-b^2)i \sin \alpha}{2b \cos \alpha - (1+b^2)i \sin \alpha}$$

$$\alpha = \frac{\omega}{c} d \left(1 - n^2 \sin^2 \theta_i\right)^{1/2}$$

$$\frac{E_2}{E_0} = \frac{b(1+b)(\cos \alpha - i \sin \alpha)}{2b \cos \alpha - i(1+b^2) \sin \alpha}$$

$$b = \frac{n \cos \theta_i}{\sqrt{1 - n^2 \sin^2 \theta_i}}$$

$$\frac{E_3}{E_0} = \frac{b(1-b)(\cos \alpha + i \sin \alpha)}{2b \cos \alpha - i(1+b^2) \sin \alpha}$$

$$\frac{E_4}{E_0} = \frac{2b}{2b \cos \alpha - i(1+b^2) \sin \alpha}$$

7.3 a), cont'd

Polarization \perp plane of incidence, cont'd

Below the critical angle of total internal reflection:

~~α, b~~ α, b are real-valued

$$\text{Reflected power } R = \left| \frac{E_1}{E_0} \right|^2 = \frac{(1-b^2)^2 \sin^2 \alpha}{4b^2 \cos^2 \alpha + (1+b^2)^2 \sin^2 \alpha}$$

$$\text{Transmitted power } T = \left| \frac{E_4}{E_0} \right|^2 = \frac{4b^2}{4b^2 \cos^2 \alpha + (1+b^2)^2 \sin^2 \alpha}$$

Above the critical angle, α, b become pure imaginary.

$$\text{Write } \alpha = i\lambda = i \frac{\omega}{c} d \sqrt{n^2 \sin^2 \theta_i - 1}$$

$$b = i\gamma = -i \frac{n \cos \theta_t}{\sqrt{n^2 \sin^2 \theta_i - 1}}$$

$$\text{Reflected power } R = \left| \frac{E_1}{E_0} \right|^2 = \frac{4\gamma^2}{4\gamma^2 \cosh^2 \lambda + (1-\gamma^2)^2 \sinh^2 \lambda}$$

7.3 d, cont'd

Polarization II plane of incidence: Here, modify $\hat{B} \parallel \hat{y}$.

$$\begin{aligned} \vec{E}_I &= (-\cos\theta_i \hat{x} + \sin\theta_i \hat{z}) E_0 e^{i\frac{\omega}{c} z \cos\theta_i} \\ &\quad + (\cos\theta_i \hat{x} + \sin\theta_i \hat{z}) E_1 e^{-i\frac{\omega}{c} z \cos\theta_i} \end{aligned}$$

$$\begin{aligned} \vec{E}_{II} &= (-\cos\theta_2 \hat{x} + n \sin\theta_i \hat{z}) E_2 e^{i\frac{\omega}{c} z \cos\theta_2} \\ &\quad + (\cos\theta_2 \hat{x} + n \sin\theta_i \hat{z}) E_3 e^{-i\frac{\omega}{c} z \cos\theta_2} \end{aligned}$$

$$\vec{E}_{III} = (-\cos\theta_i \hat{x} + \sin\theta_i \hat{z}) E_4 e^{i\frac{\omega}{c} \omega \cos\theta_i (z-d)}$$

$$\vec{B}_I = -\hat{y} \left(\frac{n}{c}\right) (E_0 e^{i\frac{\omega}{c} z \cos\theta_i} + E_1 e^{-i\frac{\omega}{c} z \cos\theta_i})$$

$$\vec{B}_{II} = -\hat{y} \left(\frac{1}{c}\right) (E_2 e^{i\frac{\omega}{c} z \cos\theta_2} + E_3 e^{-i\frac{\omega}{c} z \cos\theta_2})$$

$$\vec{B}_{III} = -\hat{y} \left(\frac{n}{c}\right) E_4 e^{i\frac{\omega}{c} \omega (z-d) \cos\theta_i}$$

Applying the same boundary conditions as before, we find

$$E_2 + E_3 = n(E_0 + E_1)$$

$$n(E_2 - E_3) = \frac{n \cos\theta_i}{\cos\theta_2} (E_0 - E_1)$$

$$n E_4 = E_2 e^{i\frac{\omega}{c} d \cos\theta_2} + E_3 e^{-i\frac{\omega}{c} d \cos\theta_2}$$

$$n \cos\theta_i E_4 = n \cos\theta_2 (E_2 e^{i\frac{\omega}{c} d \cos\theta_2} - E_3 e^{-i\frac{\omega}{c} d \cos\theta_2})$$

7.3 a), cont'd

After some algebra, one can show

$$\frac{E_1}{E_0} = \frac{i(n^4 - b^2) \sin \alpha}{2n^2 b \cos \alpha - i(n^4 + b^2) \sin \alpha} \quad b = \frac{n \cos \theta_i}{\sqrt{1 - n^2 \sin^2 \theta_i}}$$

$$\frac{E_2}{E_0} = \frac{bn(n^2 + b)(\cos \alpha - i \sin \alpha)}{2n^2 b \cos \alpha - i(n^4 + b^2) \sin \alpha} \quad \alpha = \frac{\omega d \sqrt{1 - n^2 \sin^2 \theta_i}}{c}$$

$$\frac{E_3}{E_0} = \frac{bn(n^2 - b)(\cos \alpha + i \sin \alpha)}{2n^2 b \cos \alpha - i(n^4 + b^2) \sin \alpha}$$

$$\frac{E_4}{E_0} = \frac{2n^2 b}{2n^2 b \cos \alpha - i(n^4 + b^2) \sin \alpha}$$

Below the critical angle,

$$\text{Reflected power } R = \left| \frac{E_1}{E_0} \right|^2 = \frac{(n^4 - b^2)^2 \sin^2 \alpha}{4n^4 b^2 \cos^2 \alpha + (n^4 + b^2)^2 \sin^2 \alpha}$$

$$\text{Transmitted power } T = \left| \frac{E_4}{E_0} \right|^2 = \frac{4n^4 b^2}{4n^4 b^2 \cos^2 \alpha + (n^4 + b^2)^2 \sin^2 \alpha}$$

Above the critical angle,

$$\text{define } a = \frac{\omega d \sqrt{n^2 \sin^2 \theta_i - 1}}{c}, \quad \beta = \frac{n \cos \theta_i}{\sqrt{n^2 \sin^2 \theta_i - 1}}$$

$$\text{Reflected power } R = \left| \frac{E_1}{E_0} \right|^2 = \frac{(n^4 + \beta^2)^2 \sinh^2 a}{4n^4 \beta^2 \cosh^2 a + (n^4 - \beta^2)^2 \sinh^2 a}$$

$$\text{Transmitted power } T = \left| \frac{E_4}{E_0} \right|^2 = \frac{4n^4 \beta^2}{4n^4 \beta^2 \cosh^2 a + (n^4 - \beta^2)^2 \sinh^2 a}$$

7.12 The time dependence of electrical disturbances in good conductors is governed by the frequency-dependent conductivity

$$\sigma = \frac{f_0 N e^2}{m (\gamma_0 - i\omega)} \quad (7.58)$$

Consider longitudinal electric fields in a conductor, using Ohm's law, the continuity equation, and the differential form of Coulomb's law.

a) Show that the time-Fourier-Transformed charge density satisfies the equation

$$\underline{[\sigma(\omega) - i\omega \epsilon_0] \rho(\bar{x}, \omega) = 0.}$$

$$\text{Continuity eq'n: } \nabla \cdot \bar{J} + \frac{\partial \rho}{\partial t} = 0$$

$$\text{Ohm's law: } \bar{J} = \sigma \bar{E}$$

$$\Rightarrow \sigma \nabla \cdot \bar{E} + \frac{\partial \rho}{\partial t} = 0$$

||
1/ε₀ from Gauss's law

$$\Rightarrow \frac{\sigma}{\epsilon_0} \rho + \frac{\partial \rho}{\partial t} = 0$$

$$\text{Assume } \rho(\bar{x}, t) = \frac{1}{\sqrt{2\pi}} \int d\omega \rho(\bar{x}, \omega) e^{-i\omega t}$$

$$\Rightarrow \frac{\partial \rho}{\partial t} = \frac{1}{\sqrt{2\pi}} \int d\omega (-i\omega) \rho(\bar{x}, \omega) e^{-i\omega t}$$

$$\text{As } \frac{\sigma}{\epsilon_0} \rho(\bar{x}, t) + \frac{\partial \rho}{\partial t} = \frac{1}{\sqrt{2\pi}} \int d\omega e^{-i\omega t} \left(\frac{\sigma}{\epsilon_0} \rho(\bar{x}, \omega) - i\omega \rho(\bar{x}, \omega) \right)$$

$$\Rightarrow \boxed{(\sigma - i\omega \epsilon_0) \rho(\bar{x}, \omega) = 0}$$

7.12, cont'd

b) Using the representation $\sigma(\omega) = \sigma_0 (1 - i\omega\tau)^{-1}$,
 where $\sigma_0 = \epsilon_0 \omega_p^2 \tau$ and τ is a damping time,
 show that in the approximation $\omega_p \tau \gg 1$ any initial disturbance
 will oscillate with the plasma frequency and decay in
 amplitude with a decay constant $\lambda = 1/2\tau$.

Note that if you use $\sigma(\omega) = \sigma(0) = \sigma_0$ in (a),
 you will find no oscillations & extremely rapid damping.

From (a), $\sigma(\omega) = i\epsilon_0 \omega$.

$$\Rightarrow \frac{\sigma_0}{1 - i\omega\tau} = i\epsilon_0 \omega \Rightarrow \frac{\omega_p^2 \tau}{1 - i\omega\tau} = i\omega$$

$$\Rightarrow i\omega(1 - i\omega\tau) = \omega_p^2 \tau$$

$$i\omega + \omega^2 \tau - \omega_p^2 \tau = 0$$

$$\Rightarrow \omega = \frac{-i \pm \left(\sqrt{1 - 4(\tau)(-\omega_p^2 \tau)} \right)^{1/2}}{2\tau}$$

$$= \frac{-i \pm \left(4\tau^2 \omega_p^2 - 1 \right)^{1/2}}{2\tau}$$

If $\omega_p \tau \gg 1$,

$$\omega \approx \frac{-i \pm 2\omega_p \tau}{2\tau} = \pm \omega_p - \frac{i}{2\tau}$$

\Rightarrow oscillation at plasma frequency ω_p ,
 with decay constant $\frac{1}{2\tau}$

7.16 Plane waves propagate in a homogeneous nonpneable but anisotropic dielectric. The dielectric is characterized by a tensor ϵ_{ij} , but if coordinate axes are chosen as the principal axes, the components of displacement along these axes are related to the electric field component by $D_i = \epsilon_i E_i$, where ϵ_i are the eigenvalues of the matrix ϵ_{ij} .

a) Show that plane waves with frequency ω and wavevector \mathbf{k} must satisfy

$$\mathbf{k} \times (\mathbf{k} \times \mathbf{E}) + \mu_0 \omega^2 \mathbf{D} = 0$$

This is a general result that does not depend on the form of the dielectric tensor.

Recall Maxwell's equations for harmonic fields include

$$i\mathbf{k} \times \mathbf{H} + i\omega \mathbf{D} = 0, \quad i\mathbf{k} \times \mathbf{E} - i\omega \mathbf{B} = 0$$

$$\Rightarrow i\mathbf{k} \times (i\mathbf{k} \times \mathbf{E}) - i\omega (i\mathbf{k} \times \mathbf{B}) = 0$$

$$\text{Use } \mathbf{B} = \mu_0 \mathbf{H} \Rightarrow i\mathbf{k} \times (i\mathbf{k} \times \mathbf{E}) + \mu_0 \omega^2 (\mathbf{k} \times \mathbf{H}) = 0$$

$$\Rightarrow -\mathbf{k} \times (\mathbf{k} \times \mathbf{E}) - \mu_0 \omega^2 \mathbf{D} = 0$$

7-16, cont'd

b) Show that for a given wave vector $\vec{k} = k\hat{n}$ there are two distinct modes of propagation with different phase velocities $v = \omega/k$ that satisfy the Fresnel equation

$$\sum_i \frac{n_i^2}{v^2 - v_i^2} = 0$$

where $v_i = \sqrt{\mu_0 \epsilon_i}$ is called a principal velocity, and n_i is the component of \hat{n} along the i^{th} principal axis.

Write $\vec{k} = k\hat{n}$

$$\begin{aligned} \vec{k} \times (\vec{k} \times \vec{E}) &= (\vec{k} \cdot \vec{E})\vec{k} - (k^2)\vec{E} \\ &= k^2 (\hat{n} \cdot \vec{E})\hat{n} - \vec{E} \end{aligned}$$

$$\text{Hence } \vec{k} \times (\vec{k} \times \vec{E}) + \mu_0 \omega^2 \vec{D} = 0$$

$$\Rightarrow (\hat{n} \cdot \vec{E})\hat{n} - \vec{E} + \mu_0 v^2 \vec{D} = 0$$

Work with the principal axes, and define

$$A_{ij} = n_i n_j - \delta_{ij}, \quad W_{ij} = \delta_{ij} \mu_0 \epsilon_j = \frac{\delta_{ij}}{v_j^2}$$

$$\Rightarrow A\vec{E} = -v^2 W\vec{E} \quad \text{or} \quad (A + v^2 W)\vec{E} = 0$$

Find the velocities by solving

$$0 = \det(A + v^2 W)$$

(cont'd)

7.16 b), cont'd

$$\det(A + v^2 W) = 0$$

$$= \det \begin{pmatrix} n_1^2 - 1 + v^2/v_1^2 & n_1 n_2 & n_1 n_3 \\ n_1 n_2 & n_2^2 - 1 + v^2/v_2^2 & n_2 n_3 \\ n_1 n_3 & n_2 n_3 & n_3^2 - 1 + v^2/v_3^2 \end{pmatrix}$$

$$= \left(n_1^2 + \left(\frac{v^2}{v_1^2} - 1 \right) \right) \left(\left(\frac{v^2}{v_2^2} - 1 \right) \left(\frac{v^2}{v_3^2} - 1 \right) + n_2^2 \left(\frac{v^2}{v_3^2} - 1 \right) + n_3^2 \left(\frac{v^2}{v_2^2} - 1 \right) \right) \\ - n_1 n_2 \left(n_1 n_2 \left(\frac{v^2}{v_3^2} - 1 \right) \right) + n_1 n_3 \left(-n_1 n_3 \left(\frac{v^2}{v_2^2} - 1 \right) \right)$$

$$= \left(\frac{v^2}{v_1^2} - 1 \right) \left(\frac{v^2}{v_2^2} - 1 \right) \left(\frac{v^2}{v_3^2} - 1 \right)$$

$$+ n_1^2 \left(\frac{v^2}{v_2^2} - 1 \right) \left(\frac{v^2}{v_3^2} - 1 \right) + n_2^2 \left(\frac{v^2}{v_1^2} - 1 \right) \left(\frac{v^2}{v_3^2} - 1 \right) + n_3^2 \left(\frac{v^2}{v_1^2} - 1 \right) \left(\frac{v^2}{v_2^2} - 1 \right)$$

$$+ \cancel{n_1^2 n_2^2 \left(\frac{v^2}{v_3^2} - 1 \right)} + \cancel{n_1^2 n_3^2 \left(\frac{v^2}{v_2^2} - 1 \right)}$$

$$- \cancel{n_1^2 n_2^2 \left(\frac{v^2}{v_3^2} - 1 \right)} - \cancel{n_1^2 n_3^2 \left(\frac{v^2}{v_2^2} - 1 \right)}$$

$$= \left[\prod_i \left(\frac{v^2}{v_i^2} - 1 \right) \right] \left[1 + \sum_i \frac{n_i^2}{v^2/v_i^2 - 1} \right] \Rightarrow 1 + \sum_i \frac{n_i^2}{v^2/v_i^2 - 1} = 0$$

Now, use the fact that since

$n_i = i^{\text{th}}$ component of unit vector \hat{n}

(not index of refraction in i^{th} direction),

$$\sum n_i^2 = 1$$

7.16 b), cont'd

$$\text{since } \sum n_i^2 = 1,$$

$$1 + \sum_i \frac{n_i^2}{v^2/v_i^2 - 1}$$

$$= \sum_i n_i^2 \left[1 + \frac{1}{v^2/v_i^2 - 1} \right]$$

$$= \sum_i n_i^2 \left[\frac{v^2/v_i^2 - 1 + 1}{v^2/v_i^2 - 1} \right]$$

$$= \sum_i n_i^2 \left[\frac{v^2}{v^2 - v_i^2} \right]$$

$$= v^2 \sum_i \frac{n_i^2}{v^2 - v_i^2}$$

Thus,

$$1 + \sum_i \frac{n_i^2}{v^2/v_i^2 - 1} = 0 \Rightarrow$$

$$\boxed{\sum_i \frac{n_i^2}{v^2 - v_i^2} = 0}$$

7.16, cont'd

c) Show that $\bar{D}_a \cdot \bar{D}_b = 0$, where \bar{D}_a, \bar{D}_b are the displacements associated with the two modes of propagation.

Recall from part (b) that

$$(\hat{n} \cdot \bar{E}) \hat{n} - \bar{E} + \mu_0 v^2 \bar{D} = 0 \quad \text{or} \quad (A + v^2 W) \bar{E} = 0$$

In particular,

$$(A + v_a^2 W) \bar{E}_a = 0, \quad (A + v_b^2 W) \bar{E}_b = 0$$

where v_a, v_b are the principal velocities associated with \bar{E}_a, \bar{E}_b .

$$\Rightarrow E_b^T (A + v_a^2 W) E_a = 0, \quad E_a^T (A + v_b^2 W) E_b = 0$$

Since A, W are symmetric, may transpose & take difference:

$$\Rightarrow (v_a^2 - v_b^2) E_a^T W E_b = 0$$

If $v_a \neq v_b$, then $E_a^T W E_b = 0$.

If $v_a = v_b$, then can we Gram-Schmidt to make the vectors orthogonal.

Since $W = \mu_0 \Sigma$ for $\Sigma = \text{diag}(\epsilon_1, \epsilon_2, \epsilon_3)$, & $\bar{D} = \Sigma \bar{E}$,

$$E_a^T W E_b = 0 \Rightarrow E_a \cdot \bar{D}_b = 0 \quad \text{or} \quad E_b \cdot \bar{D}_a = 0$$

$$\bar{D}_a \cdot \bar{D}_b = E_a^T \Sigma^2 E_b = \frac{1}{\mu_0^2} E_a^T W^2 E_b = \frac{1}{\mu_0^2 v_a^2 v_b^2} E_a^T A^2 E_b$$

Note $A^2 = -A$

$$\Rightarrow \bar{D}_a \cdot \bar{D}_b = -\frac{1}{\mu_0 v_a^2 v_b^2} E_a^T A E_b = +\frac{1}{\mu_0 v_a^2} E_a^T W E_b = 0$$

$$\Rightarrow \boxed{\bar{D}_a \cdot \bar{D}_b = 0} \quad (\text{However, } E_a \cdot E_b \neq 0 \text{ in general.})$$

7.28 A circularly polarized plane wave moving in the z direction for a finite extent in the x and y directions. Assuming that the amplitude modulation is slowly varying (the wave is many wavelengths broad), show that the electric and magnetic fields are given approximately by

$$\vec{E}(x, y, z, t) = \left[E_0(x, y) (\hat{e}_1 \pm i\hat{e}_2) + \frac{i}{k} \left(\frac{\partial E_0}{\partial x} \pm i \frac{\partial E_0}{\partial y} \right) \hat{e}_3 \right] e^{i(kz - \omega t)}$$

$$\vec{B} \approx \mp i \sqrt{\mu \epsilon} \vec{E}$$

where $\hat{e}_1, \hat{e}_2, \hat{e}_3$ are unit vectors in the x, y, z directions.

Because this is a circularly polarized plane wave, expect that \vec{E} is of the form

$$\vec{E} = \left[E_0(\hat{e}_1 \pm i\hat{e}_2) + F(x, y) \hat{e}_3 \right] e^{i(kz - \omega t)}$$

~~Assume~~

From Maxwell's equation, $\nabla \cdot \vec{E} = 0$

$$\Rightarrow \left(\frac{\partial E_0}{\partial x} \pm i \frac{\partial E_0}{\partial y} + ikF \right) e^{i(kz - \omega t)} = 0$$

$$\Rightarrow F = \frac{i}{k} \left(\frac{\partial E_0}{\partial x} \pm i \frac{\partial E_0}{\partial y} \right). \quad \underline{\text{Result follows.}}$$

Similarly, from Maxwell's eq'n,

$$\frac{\partial \vec{B}}{\partial t} = -\nabla \times \vec{E}$$

$$= -\hat{e}_1 \left(\frac{\partial E_y}{\partial z} - \frac{\partial E_z}{\partial y} \right) + \hat{e}_2 \left(\frac{\partial E_z}{\partial x} - \frac{\partial E_x}{\partial z} \right) - \hat{e}_3 \left(\frac{\partial E_x}{\partial y} - \frac{\partial E_y}{\partial x} \right)$$

7.28, cont'd

$$\frac{\partial \bar{B}}{\partial t} = -\hat{e}_1 \left(\frac{\partial F}{\partial y} - (\pm i) E_0 (ih) \right) e^{i(kz - \omega t)} + \hat{e}_2 \left(\frac{\partial F}{\partial x} - E_0 (ih) \right) e^{i(kz - \omega t)} - \hat{e}_3 \left(\pm i \frac{\partial E_0}{\partial x} - \frac{\partial E_0}{\partial y} \right) e^{i(kz - \omega t)}$$

Since we are told the amplitude modulation is slowly varying, we will neglect $\partial F / \partial x$, $\partial F / \partial y$, as these are second derivatives of E_0 .

$$\Rightarrow \frac{\partial \bar{B}}{\partial t} \approx -\hat{e}_1 (\pm k E_0) e^{i(kz - \omega t)} - \hat{e}_2 (ih) E_0 e^{i(kz - \omega t)} - \hat{e}_3 \left(\pm i \frac{\partial E_0}{\partial x} - \frac{\partial E_0}{\partial y} \right) e^{i(kz - \omega t)}$$

$$\Rightarrow \bar{B} \approx -\frac{ih}{\omega} \left(\pm E_0 \hat{e}_1 + i E_0 \hat{e}_2 + \frac{1}{k} \left(\pm i \frac{\partial E_0}{\partial x} - \frac{\partial E_0}{\partial y} \right) \hat{e}_3 \right) e^{i(kz - \omega t)}$$

$$= \mp \frac{ih}{\omega} \left(E_0 \hat{e}_1 \pm i E_0 \hat{e}_2 + \frac{1}{k} \left(i \frac{\partial E_0}{\partial x} \mp \frac{\partial E_0}{\partial y} \right) \hat{e}_3 \right) e^{i(kz - \omega t)}$$

$$= \mp i \sqrt{\mu \epsilon} E \left[E_0 (\hat{e}_1 \pm i \hat{e}_2) + \frac{i}{k} \left(\frac{\partial E_0}{\partial x} \pm i \frac{\partial E_0}{\partial y} \right) \hat{e}_3 \right] e^{i(kz - \omega t)}$$

$$= \mp i \sqrt{\mu \epsilon} E$$